# Performance bounds for tracking in a multipath environment

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# Outline

### Introduction

## 2 Existing work

- 3 Assumptions and extensions
- 4 Modelling and notation
- 5 Performance bounds
- 6 Future Work





Introduction

# Tracking a target in a multipath environment



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#### Conventional radar systems

Rely on Line of Sight (LOS) communication between the target and the radar head

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- Treat multipath as interference
- Radar operating in an urban environment
  - ▶ LOS is no longer guaranteed.
  - Lot of reflections from obstacles
- Modern research interests on multipath

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## Existing work

• Common assumptions (Krolik et al 2006, Chakraborty et al 2010,)

- Knowledge of the wall locations
- Knowledge of the wall reflectivities
- Knowledge of the number of targets
- Too specific geometric assumptions regarding the obstacles (eg. narrow canals)
- Detection based tracking (Barbosa et al 2008)



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# Assumptions and extensions

We derive the lower bound on the MSE under the following:

#### Common assumptions

- Target is a point scatterer
- Building locations are known
- Specular reflections at walls (reflective angle=incident angle)
- Higher order reflections are ignored
- Multiple transmitters and receivers
- Each receiver consists of a phase array antenna with L number of elements
- Extensions
  - Reflectivity of Buildings modelled as random variables
  - Each multipath is subject to a random phase shift which is distributed according to a uniform distribution
  - Tracking performed with pre-detection measurements
  - No geometrical restrictions on the wall placement

# Modelling and notation

- The state space at time *t<sub>k</sub>* could be partitioned into 3 components
  - Target dynamics;  $\mathbf{x}_k = [x_k \ \dot{x}_k \ y_k \ \dot{y}_k]'$
  - Wall and Target reflectivities;  $\mathbf{z} = [\epsilon \varepsilon_1 \cdots \varepsilon_B]'$
  - Collection of random phases that affect each path;  $\psi_k$
- Target reflectivity(ε) and building reflectivities (ε<sub>1</sub> · · · ε<sub>B</sub>) are modeled as Gaussian random parameters

#### State evolves according to;

$$\begin{aligned} \mathbf{x}_k &= \mathbf{F}_k \mathbf{x}_{k-1} + \mathbf{G}_k \mathbf{w}_k, \qquad k = 1, 2, \dots, \\ \mathbf{z} &\sim N(\mu_z, P_z) \\ \psi_k &\sim U_{(0:2\pi)^{P(\mathbf{x}_k)}} \end{aligned}$$

Where  $P(\mathbf{x}_k)$  denotes the number of multipaths at time k

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## Measurement model



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# Measurement model Contd...



# Posterior Cramer-rao lower bound (PCRB)

- Let **x** be a vector of random parameters and **y** be a vector of measured data.
- Let  $g(\mathbf{y})$  be an estimate of  $\mathbf{x}$ . The PCRB has the form

$$E[g(\mathbf{y}) - \mathbf{x}][g(\mathbf{y}) - \mathbf{x}]' \ge J^{-1}$$

Where J is the Information matrix

- Recursive method proposed by Tichavsky *et al* (1998) to obtain the PCRB
- Challenging to find the various quantities needed to apply this method for the setup we have used
- How this was done is discussed next

### Performance bounds

Let  $\bar{\mathbf{X}}_k = [\mathbf{X}'_k \ \psi'_k]^{T}$  The lower bound for MSE of estimators of  $\bar{\mathbf{X}}_k$  and  $\mathbf{Z}_k$ , denoted as  $(\mathbf{J}_k^{Z\bar{X}})^{-1}$  and  $(\mathbf{J}_k^{Z\bar{Z}})^{-1}$  could be found as;

$$\begin{split} \mathbf{J}_{k}^{Xx} &= \mathbf{H}_{k}^{33} - (\mathbf{H}_{k}^{13})'[\mathbf{J}_{k-1}^{xx} + \mathbf{H}_{k}^{11}]^{-1}\mathbf{H}_{k}^{13} \\ \mathbf{J}_{k}^{\overline{X}z} &= (\mathbf{H}_{k}^{23})' - (\mathbf{H}_{k}^{13})'[\mathbf{J}_{k-1}^{xx} + \mathbf{H}_{k}^{11}]^{-1}\mathbf{J}_{k-1}^{xz} \\ \mathbf{J}_{k}^{zz} &= \mathbf{J}_{k-1}^{zz} + \mathbf{H}_{k}^{22} - (\mathbf{J}_{k-1}^{xz})'[\mathbf{J}_{k-1}^{xx} + \mathbf{H}_{k}^{11}]^{-1}\mathbf{J}_{k-1}^{xz} \end{split}$$

where, with  $\mathbf{Q}_k = \mathbf{G}_k \mathbf{G}'_k$ ,

$$\begin{aligned} \mathbf{H}_{k}^{11} &= \operatorname{diag}(\mathbf{F}_{k}'\mathbf{Q}_{k}^{-1}\mathbf{F}_{k}, [\mathbf{0}]_{P(\mathbf{x}_{k})}) \\ \mathbf{H}_{k}^{13} &= -\operatorname{diag}(\mathbf{F}_{k}'\mathbf{Q}_{k}^{-1}, [\mathbf{0}]_{P(\mathbf{x}_{k})}) \\ \mathbf{H}_{k}^{22} &= \frac{1}{\sigma^{2}}\operatorname{Re}\{\operatorname{E}[\nabla_{\mathbf{z}_{k}}h(\cdot)'(\nabla_{\mathbf{z}_{k}}h(\cdot)^{*})']\} \\ \mathbf{H}_{k}^{23} &= \frac{1}{\sigma^{2}}\operatorname{Re}\{\operatorname{E}[\nabla_{\mathbf{z}_{k}}h(\cdot)'(\nabla_{\mathbf{\bar{x}}_{k}}h(\cdot)^{*})']\} \\ \mathbf{H}_{k}^{33} &= \operatorname{diag}(\mathbf{Q}_{k}^{-1}, [\mathbf{0}]_{\rho(\mathbf{x})_{k}}) + \frac{1}{\sigma^{2}}\operatorname{Re}\{\operatorname{E}[\nabla_{\mathbf{\bar{x}}_{k}}h(\cdot)'(\nabla_{\mathbf{\bar{x}}_{k}}h(\cdot)^{*})']\} \end{aligned}$$

with  $\nabla$  the gradient operator and  $p(\mathbf{x}_k)$  being the number of paths.

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with  $\nabla$  the gradient operator and  $p(\mathbf{x}_k)$  being the number of paths.

# **Finding derivatives**



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 We need to evaluate partial derivatives with respect to x of functions of the form:

$$f(d_1(\mathbf{x}),\ldots,d_L(\mathbf{x}),\delta_1(\mathbf{x}),\ldots,\delta_S(\mathbf{x}),\mathbf{z})$$

Where  $\delta_s$  is the distance from the *s*<sup>th</sup>reference and reflection points in the transmitter-target path

• Derivative of *f* with respect to *x* could be calculated as;

$$\frac{\partial f}{\partial x} = \sum_{i=0}^{L} \frac{\partial f}{\partial d_i} \frac{\partial d_i}{\partial x} + \sum_{j=0}^{S} \frac{\partial f}{\partial \delta_j} \frac{\partial \delta_j}{\partial x}$$

• How to calculate 
$$\frac{\partial d_i}{\partial x}$$
 and  $\frac{\partial \delta_j}{\partial x}$ ???





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• Three equations obtained

$$d_{L} = f_{L}(x, y, \theta)$$
  

$$d_{l} = f_{l}(d_{l+1}, \theta) \quad \text{for } l = 1, \dots, L-1$$
  

$$\theta = f_{0}(d_{1})$$

 Recursive relationship for the partial derivatives could be expressed as; <sup>∂d<sub>l</sub></sup>/<sub>∂x</sub> for *l* = 1,..., *L* as;

$$\frac{\partial \boldsymbol{d}_l}{\partial \boldsymbol{x}} = \alpha_l + \eta_l \frac{\partial \theta}{\partial \boldsymbol{x}}$$

with  $\alpha_l = \alpha_{l+1} \partial f_l / \partial d_{l+1}$  and  $\eta_l = \eta_{l+1} \partial f_l / \partial d_{l+1} + \partial f_l / \partial \theta$  where  $\alpha_L = \partial f_L / \partial x$  and  $\eta_L = \partial f_L / \partial \theta$ 

• Once  $\alpha_1$  and  $\eta_1$  is known  $\frac{\partial \theta}{\partial x}$  could be obtained

# Illustration



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#### • Now we can find $\alpha_0$ and $\eta_0$ and thus $\frac{\partial \theta}{\partial x}$

$$\alpha_0 = \alpha_1 \frac{\partial f_0}{\partial d_1}$$
 and  $\eta_0 = \eta_1 \frac{\partial f_0}{\partial d_1}$ 

$$\frac{\partial \theta}{\partial x} = \frac{\alpha_0}{1 - \eta_0}$$



# Performance bounds Contd...

#### **Radar scene**



# Performance bounds Contd...

#### **Results (PCRB of positions estimates)**



# Performance bounds Contd...

#### **Results (PCRB of velocity estimates)**



#### Future work

- Implement a filter for the setup introduced
- Multiple targets and possibly unknown number of targets
- Unknown locations of the obstacles
- Waveforms that would give better results
- Resource scheduling

#### Q&A

#### Thank you!